LLNL-TR-851689

Bramblett and Czirr Self-Shielded Fission Rates for ²³⁵U Physical and Analytic Benchmark



June 30, 2023

Dave Heinrichs Ed Lent Nuclear Criticality Safety Division

Lawrence Livermore National Laboratory, 7000 East Avenue, L-198, Livermore, CA, 94550

Auspices

This work performed under the auspices of the U.S. Department of Energy by Lawrence Livermore National Laboratory under Contract DE-AC52-07NA27344.

Disclaimer

This document was prepared as an account of work sponsored by an agency of the United States government. Neither the United States government nor Lawrence Livermore National Security, LLC, nor any of their employees makes any warranty, expressed or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States government or Lawrence Livermore National Security, LLC. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States government or Lawrence National Security, LLC, and shall not be used for advertising or product endorsement purposes.

Introduction:

These experiments were performed by Bramblett and Czirr at UCRL (i.e., LLNL) in the late 1960s through the 1970s and evaluated by Mark Lee (LFO, retired) for the ICSBEP Handbook. Dimensions, geometry, and benchmark RSFR values are taken from the Handbook. All sample calculational results used COG 11.3 with ENDF/B-VIII.0 cross-sections. A sample input listing is provided in Appendix A.

Modeled Surface	Distance from Source (cm)	Dimensions (cm)
Planar Disc Neutron Source	0 (origin)	diameter = 14.6
First face of HEU sample disc	100	diameter = 15
- Second face of HEU sample disc A	101.01818	diameter = 15
- Second face of HEU sample disc B	100.50658	diameter = 15
- Second face of HEU sample disc C	100.20599	diameter = 15
- Second face of HEU sample disc D	100.10524	diameter = 15
- Second face of HEU sample disc E	100.04246	diameter = 15
- Second face of HEU sample disc F	100.02695	diameter = 15
First face of HEU detector foil	500	diameter = 15
Second face of HEU detector foil	500.00030261	diameter = 15

Dimensions: Cylindrical symmetry about the x-axis



Neutron source: 1/E spectrum from 0.359 eV to 2780 eV.

Note that the relative shielded fission rate (RSFR) experimental results extend from 0.464 eV to 2150 eV which are in the resolved resonance region since the unresolved resonance region extends from 2.25 keV to 25 keV according to L. C. Leal *et al.*, "An Unresolved Resonance Evaluation for ²³⁵U," in the PHYSOR 2004 proceedings.

Materials: HEU sample discs (A-F) and detector foil

Nuclide	Weight Fraction	Atom Density atoms/barn-cm
²³⁴ U	0.0136	6.544E-04
²³⁵ U	0.9322	4.466E-02
²³⁸ U	0.0542	2.564E-03

Table 12. Composition of HEU Sample Discs A and B (assumed density 18.7 g/cm³).

Table 13. Composition of HEU Sample Discs C and D (assumed density 18.7 g/cm³).

Nuclide	Weight Fraction	Atom Density atoms/barn-cm	
²³⁴ U	0.0129	6.207E-04	
²³⁵ U	0.9313	4.462E-02	
²³⁸ U	0.0558	2.640E-03	

Table 14. Composition of HEU Sample Discs E and F (assumed density 18.7 g/cm³).

Nuclide	Weight Fraction	Atom Density atoms/barn-cm	
²³⁴ U	0.0114	5.485E-04	
²³⁵ U	0.9317	4.464E-02	
²³⁸ U	0.0569	2.692E-03	

Table 15. Composition of HEU Detector Foil (assumed density 18.7 g/cm³).

Nuclide	Weight Fraction	Atom Density atoms/barn-cm
²³⁴ U	0.012	5.774E-04
²³⁵ U	0.932	4.465E-02
²³⁸ U	0.056	2.694E-03

Neut	tron Energy	COG11.3 with ENDF/B-VIII.0			Bench	nmark
Group	Range (eV)	Sample Out*	Sample In**	RSFR	RSFR	C/E
		$8.819\text{E}10 \pm 0.0\%$	$1.736E{-}11 \pm 0.4\%$			
1	0.464 - 1.0	$5.428E04 \pm 0.0\%$	$1.073\text{E}05\pm0.4\%$	$0.020\pm0.4\%$	$0.028 \pm 10.05\%$	$0.71 \pm 10.06\%$
		$1.875\text{E}12\pm0.0\%$	$\textbf{3.808E-14} \pm \textbf{0.4\%}$			
		$9.509\text{E}10\pm0.0\%$	$1.262\text{E}10\pm0.1\%$			
2	1.0 – 2.15	$5.486E04 \pm 0.0\%$	$4.080\text{E}05\pm0.1\%$	$0.074\pm0.1\%$	$0.072 \pm 10.06\%$	$1.03\pm10.06\%$
		$\textbf{2892E-12} \pm \textbf{0.0\%}$	$4.026\text{E}13\pm0.1\%$			
		$3.426E09\pm0.0\%$	$1.179\text{E}09\pm0.2\%$			
3	2.15 – 4.64	$6.075\text{E04} \pm 0.0\%$	$7.914E-05 \pm 0.1\%$	$0.130\pm0.1\%$	$0.138 \pm 10.01\%$	$0.94 \pm 10.0\%$
		$5.167\text{E12}\pm0.0\%$	$1.437\text{E}12\pm0.1\%$			
		2.858E-07±0.1%	$4.764E-09 \pm 0.2\%$			
4	4.64 - 10.0	$3.406\text{E03}\pm0.0\%$	$9.190E-05\pm0.1\%$	$0.027\pm0.1\%$	$0.025 \pm 15.04\%$	$1.08 \pm 15.04\%$
		$\textbf{2.819E-10} \pm \textbf{0.1\%}$	$\textbf{2.743E-12} \pm \textbf{0.2\%}$			
		$1.990\text{E}10 \pm 0.0\%$	$2.940E{-}11\pm0.1\%$			
5	10.0 - 21.5	$\textbf{4.137E-03} \pm \textbf{0.0\%}$	$1.682\text{E04}\pm0.1\%$	$0.041\pm0.1\%$	$0.034 \pm 6.11\%$	$1.20\pm6.11\%$
		$8.582E10 \pm 0.2\%$	$4.040\text{E}12\pm0.2\%$			
		$1.052\text{E}09 \pm 3.2\%$	$9.866E{-}11 \pm 1.0\%$			
6	21.5 – 46.4	$6.564\text{E}04 \pm 0.1\%$	$2.786E-05 \pm 0.2\%$	$0.042\pm0.2\%$	$0.043 \pm 5.41\%$	$0.99 \pm 5.41\%$
		$1.064E{-}11 \pm 0.4\%$	$1.344\text{E}12\pm0.1\%$			
		$7.981E{-}10\pm0.7\%$	$2.778E{-}11 \pm 2.0\%$			
7	46.4 - 100	$1.573\text{E04}\pm0.1\%$	$9.491E-06 \pm 0.2\%$	$0.060\pm0.2\%$	$0.067 \pm 5.81\%$	$0.90\pm5.81\%$
		$1.001\text{E}11\pm0.6\%$	$\textbf{3.579E-13} \pm \textbf{1.2\%}$			
		$5.153\text{E09} \pm 0.5\%$	$9.098\text{E}10 \pm 1.3\%$			
8	100 – 215	$9.394\text{E}05\pm0.1\%$	$9.340\text{E06} \pm 0.3\%$	$0.099\pm0.3\%$	$0.099 \pm 5.50\%$	$1.00\pm5.51\%$
		$4.452E12\pm0.5\%$	$1.799\text{E}13\pm1.6\%$			
		$4.589E-09\pm0.6\%$	$1.484\text{E09} \pm 1.3\%$			
9	215 – 464	$7.509\text{E}05\pm0.1\%$	$1.110\text{E}05\pm0.2\%$	$0.148\pm0.2\%$	$0.159\pm2.82\%$	$0.93\pm2.83\%$
		$\textbf{4.449E-12} \pm \textbf{0.7\%}$	$\textbf{3.698E-13} \pm \textbf{2.3\%}$			
		$1.239\text{E}08 \pm 0.4\%$	$\textbf{3.701E-09} \pm \textbf{0.7\%}$			
10	464 – 1000	$5.068\text{E}05 \pm 0.1\%$	$1.088\text{E}05\pm0.2\%$	$0.215\pm0.2\%$	$0.214\pm3.70\%$	$1.00\pm3.71\%$
		$3.603E10 \pm 1.1\%$	$9.982E{-}11 \pm 2.1\%$			
		$5.701E{-}10\pm0.3\%$	$2.039\text{E}10 \pm 0.5\%$			
11	1000 – 2150	$3.131\text{E}05\pm0.1\%$	$9.474E-06\pm0.1\%$	$0.303\pm0.1\%$	$0.302\pm2.21\%$	$1.00\pm2.21\%$
		$1.228\text{E}10\pm1.3\%$	$5.153E{-}11 \pm 2.2\%$			

Benchmark-Model and Sample Results: Sample A (19.04 g/cm²)

*File: czirr-0. **File: czirr-a.

Neutron Energy		COG11.3 with ENDF/B-VIII.0			Benchmark	
Group	Range (eV)	Sample Out*	Sample In**	RSFR	RSFR	C/E
1	0.464 - 1.0	8.819E-10 ± 0.0% 5.428E-04 ± 0.0% 1.875E-12 ± 0.0%	$7.486E-05 \pm 0.1\%$	0.138±0.1%	0.152 ± 5.01%	$0.91\pm5.01\%$
2	1.0 - 2.15	9.509E-10 \pm 0.0% 5.486E-04 \pm 0.0% 2.892E-12 \pm 0.0%	$1.129E-04 \pm 0.1\%$	0.206±0.1%	0.199±5.08%	$1.03\pm5.08\%$
3	2.15 - 4.64	$\begin{array}{c} 3.426\text{E09}\pm0.0\%\\ 6.075\text{E04}\pm0.0\%\\ 5.167\text{E12}\pm0.0\% \end{array}$	$1.828E-04 \pm 0.1\%$	0.301±0.1%	0.286±6.71%	$1.05 \pm 6.71\%$
4	4.64 - 10.0	$\begin{array}{c} 2.858\text{E07}{\pm}~0.1\%\\ 3.406\text{E03}{\pm}~0.0\%\\ 2.819\text{E10}{\pm}~0.1\% \end{array}$	$2.606E-04 \pm 0.1\%$	0.077±0.1%	0.070 ± 7.55%	$1.09\pm7.55\%$
5	10.0 - 21.5	$\begin{array}{c} 1.990\text{E}10\pm0.0\%\\ 4.137\text{E}03\pm0.0\%\\ 8.582\text{E}10\pm0.2\%\end{array}$	$4.828E-04 \pm 0.0\%$	0.117±0.0%	0.103 ± 6.11%	$1.13 \pm 6.11\%$
6	21.5 – 46.4	$\begin{array}{c} 1.052\text{E-}09\pm3.2\%\\ 6.564\text{E-}04\pm0.1\%\\ 1.064\text{E-}11\pm0.4\% \end{array}$	$9.078E-05\pm0.1\%$	0.138±0.1%	0.131±4.60%	$1.06 \pm 4.60\%$
7	46.4 - 100	$\begin{array}{c} \textbf{7.981E-10} \pm \textbf{0.7\%} \\ \textbf{1.573E-04} \pm \textbf{0.1\%} \\ \textbf{1.001E-11} \pm \textbf{0.6\%} \end{array}$	$2.692E-05 \pm 0.2\%$	0.171±0.2%	0.183 ± 5.82%	$0.94\pm5.82\%$
8	100 – 215	$\begin{array}{l} 5.153\text{E-09}\pm0.5\%\\ 9.394\text{E-05}\pm0.1\%\\ 4.452\text{E-12}\pm0.5\% \end{array}$	$2.389E-05 \pm 0.2\%$	$0.254\pm0.2\%$	0.260 ± 5.50%	$0.98\pm5.50\%$
9	215 – 464	$\begin{array}{l} 4.589\text{E09} \pm 0.6\% \\ 7.509\text{E05} \pm 0.1\% \\ 4.449\text{E12} \pm 0.7\% \end{array}$	$2.545E-05 \pm 0.1\%$	$0.339\pm0.1\%$	0.336± 2.81%	$1.01 \pm 2.81\%$
10	464 – 1000	$\begin{array}{c} 1.239\text{E}08\pm0.4\%\\ 5.068\text{E}05\pm0.1\%\\ 3.603\text{E}10\pm1.1\%\end{array}$	2.244E-05 ± 0.1%	0.443±0.1%	0.440 ± 3.70%	$1.01\pm3.70\%$
11	1000 – 2150	$\begin{array}{c} 5.701\text{E}10\pm0.3\%\\ 3.131\text{E}05\pm0.1\%\\ 1.228\text{E}10\pm1.3\% \end{array}$	1.700E-05±0.1%	0.543±0.1%	0.542 ± 2.21%	1.00 ± 2.21%

Benchmark-Model and Sample Results: Sample B (9.473 g/cm²)

*File: czirr-0. **File: czirr-b.

Neut	ron Energy	COG1	1.3 with ENDF/B-VIII.	0	Bench	nmark
Group	Range (eV)	Sample Out*	Sample In**	RSFR	RSFR	C/E
1	0.464 – 1.0	$8.819E-10 \pm 0.0\%$ $5.428E-04 \pm 0.0\%$ $1.875E-12 \pm 0.0\%$	$2.411E-04 \pm 0.1\%$	0.444 ± 0.1%	0.462 ± 2.01%	$0.96\pm2.01\%$
2	1.0 - 2.15	$\begin{array}{c} 9.509\text{E}10\pm0.0\%\\ 5.486\text{E}04\pm0.0\%\\ 2.892\text{E}12\pm0.0\% \end{array}$	$2.587E-04 \pm 0.1\%$	0.472±0.1%	0.453 ± 2.03%	$1.04 \pm 2.03\%$
3	2.15 - 4.64	$\begin{array}{c} 3.426\text{E09}\pm0.0\%\\ 6.075\text{E04}\pm0.0\%\\ 5.167\text{E12}\pm0.0\% \end{array}$	$3.438E-04 \pm 0.0\%$	0.566 ± 0.0%	$\textbf{0.527} \pm \textbf{6.70\%}$	$1.07\pm6.70\%$
4	4.64 - 10.0	$\begin{array}{c} 2.858\text{E07}{\pm}0.1\%\\ 3.406\text{E03}{\pm}0.0\%\\ 2.819\text{E10}{\pm}0.1\% \end{array}$	$6.545E-04 \pm 0.0\%$	0.192±0.0%	0.179±6.51%	$1.07\pm6.51\%$
5	10.0 - 21.5	$\begin{array}{c} 1.990\text{E}10\pm0.0\%\\ 4.137\text{E}03\pm0.0\%\\ 8.582\text{E}10\pm0.2\%\end{array}$	$1.107E-03 \pm 0.0\%$	0.268±0.0%	0.233 ± 6.10%	$1.15\pm6.10\%$
6	21.5 – 46.4	$\begin{array}{c} 1.052\text{E-09}\pm3.2\%\\ 6.564\text{E-04}\pm0.1\%\\ 1.064\text{E-11}\pm0.4\% \end{array}$	$2.383E-04 \pm 0.1\%$	0.363±0.1%	0.324 ± 4.60%	$1.12 \pm 4.60\%$
7	46.4 - 100	$\begin{array}{c} \textbf{7.981E-10} \pm \textbf{0.7\%} \\ \textbf{1.573E-04} \pm \textbf{0.1\%} \\ \textbf{1.001E-11} \pm \textbf{0.6\%} \end{array}$	$6.445E-05 \pm 0.2\%$	$0.410\pm0.2\%$	0.420 ± 5.80%	0.98±5.80%
8	100 – 215	$\begin{array}{l} 5.153\text{E-09}\pm0.5\%\\ 9.394\text{E-05}\pm0.1\%\\ 4.452\text{E-12}\pm0.5\% \end{array}$	$\textbf{4.893E-05} \pm \textbf{0.1\%}$	$0.520\pm0.1\%$	0.524 ± 5.50%	$0.99\pm5.50\%$
9	215 – 464	$\begin{array}{l} 4.589\text{E09}{\pm}0.6\%\\ 7.509\text{E05}{\pm}0.1\%\\ 4.449\text{E12}{\pm}0.7\%\end{array}$	$4.597\text{E}05 \pm 0.1\%$	$0.612\pm0.1\%$	0.613± 2.80%	$1.00\pm2.80\%$
10	464 – 1000	$\begin{array}{c} 1.239\text{E}08\pm0.4\%\\ 5.068\text{E}05\pm0.1\%\\ 3.603\text{E}10\pm1.1\%\end{array}$	3.585E-05 ± 0.1%	0.707±0.1%	0.703 ± 3.71%	1.01 ± 3.71%
11	1000 – 2150	$5.701E-10 \pm 0.3\% \\ 3.131E-05 \pm 0.1\% \\ 1.228E-10 \pm 1.3\%$	2.426E-05 ± 0.1%	0.775 ± 0.1%	0.773 ± 2.20%	1.00 ± 2.20%

Benchmark-Model and Sample Results: Sample C (3.852 g/cm²)

*File: czirr-0. **File: czirr-c.

$1.12 \pm 6.10\%$ Neutron		COG11.3 with ENDF/B-VIII.0			Benchmark	
Group	Range (eV)	Sample Out*	Sample Out* Sample In** RSFR		RSFR	C/E
1	0.464 – 1.0	$\begin{array}{c} 8.819\text{E}10 \pm 0.0\% \\ 5.428\text{E}04 \pm 0.0\% \\ 1.875\text{E}12 \pm 0.0\% \end{array}$	$3.579E-04 \pm 0.1\%$	0.659±0.1%	$0.662 \pm 2.01\%$	$1.00\pm2.01\%$
2	1.0 - 2.15	$\begin{array}{l} 9.509\text{E}10\pm0.0\%\\ 5.486\text{E}04\pm0.0\%\\ 2.892\text{E}12\pm0.0\% \end{array}$	$3.657E-04 \pm 0.1\%$	0.667±0.1%	0.672 ± 2.02%	$0.99\pm2.02\%$
3	2.15 - 4.64	$\begin{array}{l} 3.426\text{E09}\pm0.0\%\\ 6.075\text{E04}\pm0.0\%\\ 5.167\text{E12}\pm0.0\% \end{array}$	$4.455E-04 \pm 0.0\%$	0.733±0.0%	$\textbf{0.719} \pm \textbf{4.00\%}$	$1.02\pm4.00\%$
4	4.64 - 10.0	$\begin{array}{l} 2.858\text{E07} \pm 0.1\% \\ 3.406\text{E03} \pm 0.0\% \\ 2.819\text{E10} \pm 0.1\% \end{array}$	1.068E-03± 0.0%	$0.314\pm0.0\%$	$0.297\pm6.51\%$	$1.06\pm6.51\%$
5	10.0 - 21.5	$\begin{array}{c} 1.990\text{E}10\pm0.0\%\\ 4.137\text{E}03\pm0.0\%\\ 8.582\text{E}10\pm0.2\%\end{array}$	$1.625E-03 \pm 0.0\%$	0.393 ± 0.0%	0.352 ± 6.10%	$\textbf{1.12}\pm\textbf{6.10\%}$
6	21.5 – 46.4	$\begin{array}{c} 1.052\text{E-09}\pm3.2\%\\ 6.564\text{E-04}\pm0.1\%\\ 1.064\text{E-11}\pm0.4\% \end{array}$	$3.657E-04 \pm 0.1\%$	$0.557\pm0.1\%$	0.477 ± 4.61%	$1.17\pm4.61\%$
7	46.4 - 100	$\begin{array}{c} \textbf{7.981E-10} \pm \textbf{0.7\%} \\ \textbf{1.573E-04} \pm \textbf{0.1\%} \\ \textbf{1.001E-11} \pm \textbf{0.6\%} \end{array}$	$9.476E-05\pm0.1\%$	$0.602\pm0.1\%$	$0.605\pm5.81\%$	$1.00\pm5.81\%$
8	100 – 215	$\begin{array}{l} 5.153\text{E-09}\pm0.5\%\\ 9.394\text{E-05}\pm0.1\%\\ 4.452\text{E-12}\pm0.5\%\end{array}$	$6.565E-05\pm0.1\%$	$0.699\pm0.1\%$	$0.719\pm5.50\%$	$\textbf{0.97} \pm \textbf{5.50\%}$
9	215 – 464	$\begin{array}{l} 4.589\text{E09} \pm 0.6\% \\ 7.509\text{E05} \pm 0.1\% \\ 4.449\text{E12} \pm 0.7\% \end{array}$	$5.770E-05 \pm 0.1\%$	$0.768 \pm 0.1\%$	0.780± 2.80%	$\textbf{0.99} \pm \textbf{2.80\%}$
10	464 – 1000	$\begin{array}{c} 1.239\text{E08} \pm 0.4\% \\ 5.068\text{E05} \pm 0.1\% \\ 3.603\text{E10} \pm 1.1\% \end{array}$	$4.228E05\pm0.1\%$	$0.834\pm0.1\%$	0.841±3.71%	$\textbf{0.99} \pm \textbf{3.71\%}$
11	1000 – 2150	$\begin{array}{l} 5.701\text{E}10\pm0.3\%\\ 3.131\text{E}05\pm0.1\%\\ 1.228\text{E}10\pm1.3\%\end{array}$	$2.754E-05 \pm 0.1\%$	$0.880\pm0.1\%$	0.847 ± 2.20%	$1.04\pm2.20\%$

Benchmark-Model and Sample Results: Sample D (1.968 g/cm²)

*File: czirr-0. **File: czirr-d.

$1.12 \pm 6.10\%$ Neutron Energy		COG11.3 with ENDF/B-VIII.0			Benchmark	
Group	Range (eV)	Sample Out*	Sample In**	RSFR	RSFR	C/E
1	0.464 – 1.0	$\begin{array}{l} 8.819\text{E}10\pm0.0\%\\ 5.428\text{E}04\pm0.0\%\\ 1.875\text{E}12\pm0.0\% \end{array}$	4.585–04±0.1%	0.845±0.1%	0.848±2.01%	$1.00\pm2.01\%$
2	1.0 - 2.15	$\begin{array}{l} 9.509\text{E}10\pm0.0\%\\ 5.486\text{E}04\pm0.0\%\\ 2.892\text{E}12\pm0.0\% \end{array}$	$4.625 04 \pm 0.1\%$	0.843±0.1%	0.840±2.01%	$1.00\pm2.01\%$
3	2.15 - 4.64	$\begin{array}{l} 3.426\text{E09}\pm0.0\%\\ 6.075\text{E04}\pm0.0\%\\ 5.167\text{E12}\pm0.0\%\end{array}$	$5.334-04 \pm 0.0\%$	0.878±0.0%	$\textbf{0.874} \pm \textbf{4.00\%}$	$1.00\pm4.00\%$
4	4.64 - 10.0	$\begin{array}{c} 2.858\text{E07}{\pm}~0.1\%\\ 3.406\text{E03}{\pm}~0.0\%\\ 2.819\text{E10}{\pm}~0.1\%\end{array}$	$1.784-03 \pm 0.0\%$	0.524±0.0%	$0.514\pm6.52\%$	$\textbf{1.02} \pm \textbf{6.52\%}$
5	10.0 - 21.5	$\begin{array}{c} 1.990\text{E}10\pm0.0\%\\ 4.137\text{E}03\pm0.0\%\\ 8.582\text{E}10\pm0.2\%\end{array}$	2.399–03 ± 0.0%	0.580 ± 0.0%	$0.524 \pm 6.11\%$	$\textbf{1.11} \pm \textbf{6.11\%}$
6	21.5 – 46.4	$\begin{array}{c} 1.052\text{E}09\pm3.2\%\\ 6.564\text{E}04\pm0.1\%\\ 1.064\text{E}11\pm0.4\%\end{array}$	$5.055-04 \pm 0.1\%$	0.770±0.1%	0.693±4.61%	$1.11\pm4.61\%$
7	46.4 - 100	$\begin{array}{c} \textbf{7.981E-10} \pm \textbf{0.7\%} \\ \textbf{1.573E-04} \pm \textbf{0.1\%} \\ \textbf{1.001E-11} \pm \textbf{0.6\%} \end{array}$	$1.265-04 \pm 0.1\%$	0.804±0.1%	0.785 ± 5.80%	$1.02\pm5.80\%$
8	100 – 215	$\begin{array}{l} 5.153\text{E09}\pm0.5\%\\ 9.394\text{E05}\pm0.1\%\\ 4.452\text{E12}\pm0.5\%\end{array}$	$8.075-05 \pm 0.1\%$	$0.860 \pm 0.1\%$	$0.867 \pm 5.50\%$	$\textbf{0.99} \pm \textbf{5.50\%}$
9	215 – 464	$\begin{array}{l} 4.589\text{E09}{\pm}~0.6\%\\ 7.509\text{E05}{\pm}~0.1\%\\ 4.449\text{E12}{\pm}~0.7\%\end{array}$	$6.725-05 \pm 0.1\%$	$0.896 \pm 0.1\%$	0.894± 2.80%	$\textbf{1.00} \pm \textbf{2.80\%}$
10	464 – 1000	$\begin{array}{c} 1.239\text{E08} \pm 0.4\% \\ 5.068\text{E05} \pm 0.1\% \\ 3.603\text{E10} \pm 1.1\% \end{array}$	$4.70805\pm0.1\%$	$0.929\pm0.1\%$	$0.932 \pm 3.70\%$	$\textbf{1.00} \pm \textbf{3.70\%}$
11	1000 – 2150	$\begin{array}{c} \text{5.701E-10} \pm 0.3\% \\ \text{3.131E-05} \pm 0.1\% \\ \text{1.228E-10} \pm 1.3\% \end{array}$	2.973–05±0.1%	$0.950\pm0.1\%$	0.919 ± 2.20%	$1.03\pm2.20\%$

Benchmark-Model and Sample Results: Sample E (0.794 g/cm²)

*File: czirr-0. **File: czirr-e.

$1.12 \pm 6.10\%$ Neutron Energy		COG11.3 with ENDF/B-VIII.0			Benchmark	
Group	Range (eV)	Sample Out*	Sample In**	RSFR	RSFR	C/E
1	0.464 – 1.0	$\begin{array}{l} 8.819\text{E}10\pm0.0\%\\ 5.428\text{E}04\pm0.0\%\\ 1.875\text{E}12\pm0.0\% \end{array}$	$4.877E-04 \pm 0.1\%$	0.898±0.1%	$0.880 \pm 2.01\%$	$1.02 \pm 2.01\%$
2	1.0 - 2.15	$\begin{array}{c} 9.509\text{E}10\pm0.0\%\\ 5.486\text{E}04\pm0.0\%\\ 2.892\text{E}12\pm0.0\% \end{array}$	$4.920E-04 \pm 0.1\%$	0.897±0.1%	0.898±2.01%	$1.00 \pm 2.01\%$
3	2.15 - 4.64	$\begin{array}{l} 3.426\text{E09}\pm0.0\%\\ 6.075\text{E04}\pm0.0\%\\ 5.167\text{E12}\pm0.0\%\end{array}$	$5.586E-04 \pm 0.0\%$	0.920±0.0%	$\textbf{0.924} \pm \textbf{2.01\%}$	$1.00\pm2.01\%$
4	4.64 - 10.0	$\begin{array}{l} 2.858\text{E07} \pm 0.1\% \\ 3.406\text{E03} \pm 0.0\% \\ 2.819\text{E10} \pm 0.1\% \end{array}$	$2.165E-03 \pm 0.0\%$	0.636±0.0%	0.631± 2.05%	$1.01 \pm 2.05\%$
5	10.0 - 21.5	$\begin{array}{c} 1.990\text{E}10\pm0.0\%\\ 4.137\text{E}03\pm0.0\%\\ 8.582\text{E}10\pm0.2\%\end{array}$	2.803E-03± 0.0%	0.678±0.0%	0.640± 2.05%	$1.06\pm2.05\%$
6	21.5 – 46.4	$\begin{array}{c} 1.052\text{E-09}\pm3.2\%\\ 6.564\text{E-04}\pm0.1\%\\ 1.064\text{E-11}\pm0.4\% \end{array}$	$5.531E-04 \pm 0.1\%$	0.843±0.1%	0.793 ± 2.03%	$1.06 \pm 2.03\%$
7	46.4 - 100	$\begin{array}{c} \textbf{7.981E-10} \pm \textbf{0.7\%} \\ \textbf{1.573E-04} \pm \textbf{0.1\%} \\ \textbf{1.001E-11} \pm \textbf{0.6\%} \end{array}$	$1.364E-04 \pm 0.1\%$	$0.867\pm0.1\%$	0.865 ± 2.02%	$1.00\pm2.02\%$
8	100 – 215	$\begin{array}{l} 5.153\text{E09} \pm 0.5\% \\ 9.394\text{E05} \pm 0.1\% \\ 4.452\text{E12} \pm 0.5\% \end{array}$	$8.504E-05 \pm 0.1\%$	$0.905\pm0.1\%$	$0.898 \pm 2.01\%$	$1.01\pm2.01\%$
9	215 – 464	$\begin{array}{l} 4.589\text{E09} \pm 0.6\% \\ 7.509\text{E05} \pm 0.1\% \\ 4.449\text{E12} \pm 0.7\% \end{array}$	$7.003E05\pm0.1\%$	0.933±0.1%	0.941±2.01%	$0.99 \pm 2.01\%$
10	464 – 1000	$\begin{array}{c} 1.239\text{E08} \pm 0.4\% \\ 5.068\text{E05} \pm 0.1\% \\ 3.603\text{E10} \pm 1.1\% \end{array}$	$4.845E05\pm0.1\%$	$0.956\pm0.1\%$	$0.939 \pm 2.04\%$	$1.02\pm2.04\%$
11	1000 – 2150	$\begin{array}{l} 5.701\text{E}10\pm0.3\%\\ 3.131\text{E}05\pm0.1\%\\ 1.228\text{E}10\pm1.3\%\end{array}$	3.031E-05±0.1%	$0.968 \pm 0.1\%$	0.938±2.01%	$1.03\pm2.01\%$

Benchmark-Model and Sample Results: Sample F (0.504 g/cm²)

*File: czirr-0. **File: czirr-f.

Conclusions:

While there are ²³⁴U and ²³⁸U fissions in the detector, they are negligible in comparison to ²³⁵U fissions as shown in the tables for the results with the sample out. Therefore, only ²³⁵U fissions are reported in other table entries.

The bias in calculated results is given in the table below using the bias statistic, $x = (C/E - 1)/\sigma$. These results are noted as excellent and in good agreement with a normal distribution with a slight positive mean bias. It may be that there is increasing under-prediction with increasing sample thickness but there are too few samples to make such a conclusion definitive.

Sample	x < -3	-3 ≤ x < -2	-2 ≤ x < -1	-1 ≤ x < 0	$0 \le x \le 1$	1 < x ≤ 2	2 < x ≤ 3	3 < x ≤ 4
А		1	1	2	5		1	1
В			2	1	5	2	1	
С			1	2	3	3	2	
D				4	4	2		1
E				1	7	2	1	
F				1	7	1	2	
All		1	4	11	31	10	7	2

Table 1. Bias statistic, $x = (C/E - 1)/\sigma$

This shift to increasing under-prediction with increasing sample thickness may also seen in the bias statistic, y = C/E, shown in the following table. Further, increasing uncertainties with increasing sample thickness are evident.

	· •	
Sample	C/E	Uncertainty (%)
A	0.71 – 1.20	2.21 - 10.06
В	0.91 - 1.13	2.21 – 7.55
C	0.96 – 1.15	2.01 - 6.70
D	0.97 – 1.17	2.01 - 6.51
E	0.99 – 1.11	2.01 - 6.52
F	0.99 - 1.06	2.01 – 2.05
All	0.71 – 1.20	2.01 - 10.06

Table 2. Statistic, y = C/E

Bramblett and Czirr (1969) state: "In the geometry used in this experiment, a neutron scattered by the absorber will not strike the detector." This appears to be rigorously true as shown by comparing the results with no sample present to those with the thinnest samples present. With the thickest samples, we note increased scattering and multiplication. However, even with these few scattering events only some of which are inelastic, the spectrum is expected to be substantially unaltered. This benchmark is therefore also a valuable analytic benchmark as discussed further in Appendix B.

Sample	Percentage	N.4			
	0	1	2	3+	IVI
None	4.86	95.00	0.14		1.001
F	5.13	94.67	0.20		1.107
E	4.97	94.45	0.58		1.157
D	4.92	94.38	0.69	0.01	1.325
C	4.93	94.53	0.47	0.07	1.531
В	6.73	90.46	1.96	0.85	1.942
А	8.22	78.82	7.52	0.95	2.356

Table 3. Total Response as a Func	tion of Scattering Events Since Source Generation and
	Multiplication (M)

Note that k-eff can be calculated as the ratio of the production rate (P) to the removal rate (R), or k-eff = P/R. Therefore, M = 1/(1 - k-eff) = 1/(1 - P/R).

References

R. L. Bramblett and J. B. Czirr, "Energy-Dependent Shielding Factors for ²³⁵U Foils from Transmission Experiments," Nuclear Science and Engineering: **35**, 350-357 (1969).

J. B. Czirr and R. L. Bramblett, "Measurement of Fissions Produced in Bulk Pu²³⁹ and U²³⁵ by 2 eV to 10 keV Neutrons," UCRL-14613, Lawrence Livermore National Laboratory, December 17, 1965.

J. Czirr and R. Bramblett, "Measurement of Fissions Produced in Bulk Plutonium-239 by 2-eV to 10-keV Neutrons," Nuclear Science and Engineering: **28**, 62-71 (1967).

Mark A. Lee, International Handbook of Evaluated Criticality Safety Benchmark Experiments, Volume IX, FUND-LLNL-1/E-U235-TRANS-001, "Self-Shielded Fission Rates for ²³⁵U," September 30, 2007, NEA No. 7592, NEA/NSC/DOC(95)03, © OECD 2022.

E. F. Plechaty and D. E. Cullen, "Calculation of Resonance Self Shielding in U²³⁵," UCID-16359, Lawrence Livermore National Laboratory, June 28, 1973.

L. J. Bacon, "A Comparison of Experimental Data from Energy-Dependent Resonance Self-Shielding Factors for ²³⁵U and ²³⁹Pu with Calculations from TART," UCID-16308, Lawrence Livermore National Laboratory, November 29, 1973.

A. A. Van'kov *et al.*, "Determination of the Details of the Resonance Structure of Both the Total Cross Section and the Fission Cross Section of 235U and 239Pu for 2 eV – 20 keV Neutrons," Atomnaya Energiya: **48** (6) 377-381 (1980).

Appendix A

Sample COG 11.3 Input Deck

```
FUND-LLNL-1/E-U235-TRANS-001, Self-Shielded Fission Rates for 235U: Sample F In
basic
  neutron delayedn MEV URRPT
source
                                                       $
  npart=1E+8
  define position = 1 ss-disk 0 0 0 5 0 0 7.3
                                                       $ 7.3 cm radius disk source at x=0
  define angle
                = 1 normal fixed
                                                       $ uniform normal along +x axis
  define energy
                 = 1 neutron one/e 3.590E-7 2.780E-3
                                                       $ 1/E spectrum
  define time
                 = 1 steady
                                                       $
  increment 1 position=1 angle=1 energy=1 time=1
mix nlib=ENDFB8R0 ptlib=PT.ENDFB8R0.ACE
   mat=1 w-p 18.7 u234 0.0114 u235 0.9317 u238 0.0569
                                                       $ Sample F
                                                       $ Fission chamber detector foil
   mat=2 w-p 18.7 u234 0.012 u235 0.932 u238 0.056
  mat=24 u234 0.2244
                                                       $ For U-234 fissions in the detector
  mat=25 u235 17.4284
                                                       $ For U-235 fissions in the detector
  mat=28 u238 1.0472
                                                       $ For U-238 fissions in the detector
assign-mc
   1 red 2 blue
geometry
  sector 1 Sample -1
  sector 2 DetFoil -2
  boundary vacuum
                    3
picture cs material -10 0 10 -10 0 -10 510 0 -10 title="axial view"
surfaces
  1 c x 7.5 100.0 100.02695
                               $ Sample F
  2 c x 7.5 500.0 500.00030261 $ Fission chamber detector foil
  3 c x 8.0 -10.0 510.0
                               $ Boundary condition
detector
number = U234 title="U234 Fissions in Fission Chamber" reaction 2 5.347560E-2 DRF-E neutron R-RATE 24 15
  bin E neutron 4.64e-7 1e-6 2.15e-6 4.64e-6 1.e-5 2.15e-5 4.64e-5 1e-4 2.15e-4 4.64e-4 1e-3 2.15e-3
number = U235 title="U235 Fissions in Fission Chamber" reaction 2 5.347560E-2 DRF-E neutron R-RATE 25 15
 bin E neutron 4.64e-7 1e-6 2.15e-6 4.64e-6 1.e-5 2.15e-5 4.64e-5 1e-4 2.15e-4 4.64e-4 1e-3 2.15e-3
number = U238 title="U238 Fissions in Fission Chamber" reaction 2 5.347560E-2 DRF-E neutron R-RATE 28 15
  bin E neutron 4.64e-7 1e-6 2.15e-6 4.64e-6 1.e-5 2.15e-5 4.64e-5 1e-4 2.15e-4 4.64e-4 1e-3 2.15e-3
```

end

Appendix B

Analytic Benchmark

Since $\phi = 1/E$, the relative shielding fission rate in each group can be expressed analytically as:

$$R(x,G) = \frac{\int_{E_G}^{2.15E_G} \sigma_F(E) \exp\left[-\Sigma_T(E) x\right] \frac{dE}{E}}{\int_{E_G}^{2.15E_G} \sigma_F(E) \frac{dE}{E}}$$

Ed Lent has integrated the ENDF/B-VIII.0 cross-sections numerically and compared these analytic results to COG Monte-Carlo calculations, which are in excellent agreement with the ratio |COG/Cal| < 2% in all cases. These results are also compared to benchmark (experimental) values in the following plots, which shows the energies where the cross-section needs improvement (e.g., $0.464 \le E \le 2.15 \text{ eV}$) and where it appears to be excellent (e.g., $E \ge 21.5 \text{ eV}$).

Energy (eV)	Sample Thickness	Exp + DExp	Experiment	Exp- Dexp	Numerical Calcultion	COG	COG/Cal
0.464 - 1.	19.04	0.031	0.028	0.025	0.0182	0.0182	1.0000
	9.473	0.160	0.152	0.144	0.1315	0.1317	1.0023
	3.852	0.471	0.462	0.453	0.4346	0.4346	1.0000
	1.968	0.675	0.662	0.649	0.6419	0.6523	1.0162
	0.794	0.865	0.848	0.831	0.8412	0.8412	1.0000
	0.504	0.898	0.880	0.862	0.8960	0.8961	1.0001
1 2.15	19.04	0.079	0.072	0.065	0.0607	0.0608	1.0016
	9.473	0.209	0.199	0.189	0.1787	0.1791	1.0022
	3.852	0.462	0.453	0.444	0.4424	0.4429	1.0011
	1.968	0.686	0.672	0.658	0.6452	0.6461	1.0014
	0.794	0.857	0.840	0.823	0.8334	0.8338	1.0005
	0.504	0.916	0.898	0.880	0.8900	0.8904	1.0004
2.15 - 4.64	19.04	0.152	0.131	0.124	0.1373	0.1373	1.0000
	9.473	0.305	0.286	0.267	0.3138	0.3138	1.0000
	3.852	0.562	0.527	0.492	0.5796	0.5800	1.0007
	1.968	0.748	0.719	0.690	0.7435	0.7442	1.0009
	0.794	0.909	0.874	0.839	0.8827	0.8832	1.0006
	0.504	0.943	0.924	0.905	0.9231	0.9228	0.9997
4.64 - 10.	19.04	0.029	0.025	0.021	0.0296	0.0297	1.0034
	9.473	0.075	0.070	0.065	0.0826	0.0828	1.0024
	3.852	0.191	0.179	0.167	0.2026	0.2030	1.0020
	1.968	0.311	0.297	0.278	0.3261	0.3270	1.0028
	0.794	0.548	0.514	0.480	0.5359	0.5364	1.0009
	0.504	0.644	0.631	0.618	0.6460	0.6462	1.0003

10 21.5	19.04	0.036	0.034	0.032	0.0398	0.0399	1.0025
	9.473	0.109	0.103	0.097	0.1138	0.1142	1.0035
	3.852	0.247	0.233	0.219	0.2609	0.2613	1.0015
	1.968	0.373	0.352	0.331	0.3839	0.3844	1.0013
	0.794	0.556	0.524	0.492	0.5720	0.5723	1.0005
	0.504	0.653	0.640	0.627	0.6708	0.6719	1.0016
21.5 - 46.4	19.04	0.045	0.043	0.041	0.0428	0.0429	1.0023
	9.473	0.137	0.131	0.125	0.1290	0.1293	1.0023
	3.852	0.339	0.324	0.309	0.3160	0.3163	1.0010
	1.968	0.499	0.477	0.455	0.4887	0.4889	1.0004
	0.794	0.725	0.693	0.661	0.7154	0.7105	0.9932
	0.504	0.809	0.793	0.777	0.8021	0.7962	0.9926
46.4 - 100.	19.04	0.071	0.067	0.063	0.0605	0.0606	1.0016
	9.473	0.194	0.183	0.172	0.1717	0.1719	1.0012
	3.852	0.444	0.420	0.394	0.4101	0.4105	1.0010
	1.968	0.640	0.605	0.570	0.6039	0.6037	0.9997
	0.794	0.831	0.785	0.739	0.8030	0.8025	0.9994
	0.504	0.882	0.865	0.848	0.8675	0.8677	1.0002
100 215.	19.04	0.104	0.099	0.094	0.0987	0.0991	1.0041
	9.473	0.274	0.260	0.246	0.2532	0.2541	1.0036
	3.852	0.553	0.524	0.495	0.5207	0.5225	1.0035
	1.968	0.759	0.719	0.679	0.6991	0.7008	1.0024
	0.794	0.915	0.867	0.819	0.8580	0.8604	1.0028
	0.504	0.916	0.898	0.880	0.9055	0.9082	1.0030
215 464.	19.04	0.163	0.159	0.155	0.1474	0.1482	1.0054
	9.473	0.345	0.336	0.327	0.3373	0.3395	1.0065
	3.852	0.630	0.613	0.596	0.6095	0.6132	1.0061
	1.968	0.802	0.780	0.758	0.7657	0.7706	1.0064
	0.794	0.919	0.894	0.869	0.8925	0.8974	1.0055
	0.504	0.960	0.941	0.922	0.9284	0.9329	1.0048
464 1000.	19.04	0.222	0.214	0.206	0.2122	0.2148	1.0123
	9.473	0.456	0.440	0.424	0.4367	0.4427	1.0137
	3.852	0.729	0.703	0.677	0.6980	0.7077	1.0139
	1.968	0.872	0.841	0.810	0.8247	0.8341	1.0114
	0.794	0.966	0.932	0.898	0.9177	0.9279	1.0111
	0.504	0.958	0.939	0.920	0.9426	0.9548	1.0129
1000 2150.	19.04	0.309	0.302	0.295	0.3005	0.3020	1.0050
	9.473	0.554	0.542	0.530	0.5391	0.5409	1.0033
	3.852	0.790	0.773	0.756	0.7721	0.7759	1.0049
	1.968	0.866	0.847	0.828	0.8735	0.8766	1.0035
	0.794	0.939	0.919	0.899	0.9441	0.9478	1.0039
	0.504	0.957	0.938	0.919	0.9625	0.9662	1.0038











